

6. Second Order Design

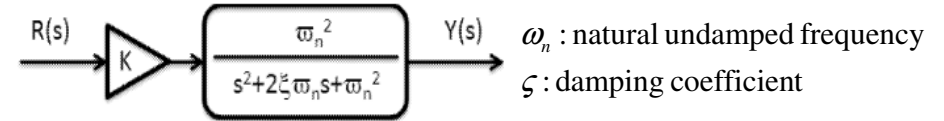
EN 2142 Electronic Control Systems



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Second Order Systems

- General second order system



- Transfer function $G_{g2}(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$

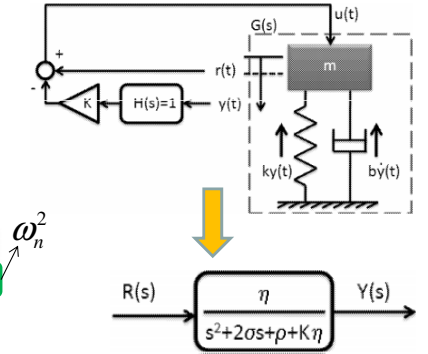
- Eg: Height adjustable stabilized platform

$$G_c(s) = \frac{\eta / (s^2 + 2\sigma s + \rho)}{1 + K\eta / (s^2 + 2\sigma s + \rho)}$$

$$= \frac{\eta}{s^2 + 2\sigma s + \rho + K\eta}$$

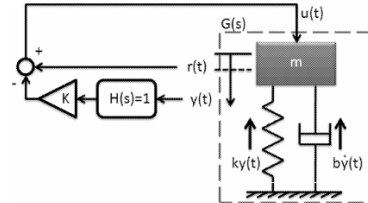
where $\eta = 1/m$, $\sigma = \frac{b}{2m}$ and $\rho = k/m$

$$\frac{Y(s)}{R(s)} = \frac{1}{k+K} \cdot \frac{\frac{(k+K)/m}{s^2 + \frac{(b/m)}{2}s + \frac{(k+K)/m}}{2\zeta\omega}}{\omega_n^2}$$



ζ and ω_n

$$m, k, b \begin{cases} \omega_n = \sqrt{\frac{k+K}{m}} \\ \zeta = \frac{b}{2\sqrt{m(k+K)}} \end{cases}$$



- DCG of the Generic 2nd order system

$$\frac{Y(s)}{R(s)} = \frac{1}{k+K} \frac{(k+K)/m}{s^2 + (b/m)s + (k+K)/m}$$

$$DCG = \lim_{s \rightarrow 0} s \frac{(k+K)/m}{s^2 + (b/m)s + (k+K)/m} = 1$$

$$DCG = \frac{1}{k+K}$$

ζ Determines the Response

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

- Poles $s_1, s_2 = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$

- Response

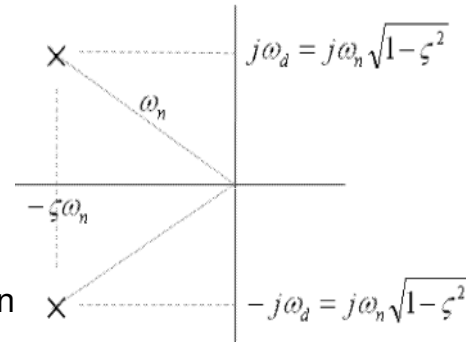
1. $\zeta > 1$ over damped (slow, no oscillations)
2. $\zeta = 1$ critically damped (quickest, nonoscillatory)
3. $0 < \zeta < 1$ under damped (damped oscillations)
4. $\zeta = 0$ stable sustained oscillations (simple harmonic motion)
5. $\zeta < 0$ unstable response

0 <math>\zeta < 1</math> Most Common In Industry

- Under Damped Response
- Poles

$$s_1, s_2 = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$$

$$= -\zeta\omega_n \pm j\omega_d$$



- Under damped transfer function

$$G_2(s) = \frac{\omega_n^2}{(s + \zeta\omega_n + j\omega_d)(s + \zeta\omega_n - j\omega_d)}$$

$$= \frac{\omega_n^2}{(s + \zeta\omega_n)^2 + \omega_d^2}$$

$$= \frac{\omega_n^2}{\omega_d} \frac{\omega_d}{(s + \zeta\omega_n)^2 + \omega_d^2}$$

Unit Step Response (0 <math>\zeta < 1</math>)

$$Y(s) = \frac{\omega_n^2}{\omega_d} \frac{\omega_d}{(s + \zeta\omega_n)^2 + \omega_d^2} \cdot \frac{1}{s} \quad y(t) = \int e^{-\zeta\omega_n t} \sin(\omega_d t) dt$$

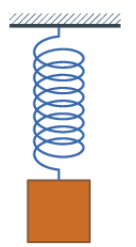
Exponential scaling in time

Integration

$$y(t) = \frac{\omega_n^2}{\omega_d} \left[\frac{\omega_d}{\omega_d^2 + \zeta^2\omega_n^2} - \frac{e^{-\zeta\omega_n t}}{\sqrt{\omega_d^2 + \zeta^2\omega_n^2}} \sin(\omega_d t + \phi) \right]$$

$$\phi = \frac{\omega_d}{\zeta\omega_n} = \frac{\sqrt{1-\zeta^2}}{\zeta}$$

Appendix B



- Because $\omega_d = \omega_n\sqrt{1-\zeta^2}$

$$y(t) = \frac{\omega_n^2}{\omega_d} \left[\frac{\omega_d}{\omega_n^2} - \frac{e^{-\zeta\omega_n t}}{\omega_n} \sin(\omega_d t + \phi) \right]$$

$$= 1 - \frac{e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} \sin(\omega_d t + \phi)$$

Peak time

Peak time t_p is the time the response takes to reach its first peak

$$\dot{y}(t) = -\frac{1}{\sqrt{1-\zeta^2}} \left[\omega_d e^{-\zeta\omega_n t} \cos(\omega_d t + \phi) - \sin(\omega_d t + \phi) e^{-\zeta\omega_n t} \zeta\omega_n \right]$$

$$= \frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \left[\zeta \sin(\omega_d t + \phi) - \sqrt{1-\zeta^2} \cos(\omega_d t + \phi) \right]$$

$$= \frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin(\omega_d t + \phi - \phi)$$

$$= \frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin(\omega_d t) \quad (5.11)$$

when $t = t_p$ $\dot{y}(t)=0$, therefore $\sin(\omega_d t_p)=0$

$$\omega_d t_p = \pi$$

$$\omega_n \sqrt{1-\zeta^2} t_p = \pi$$

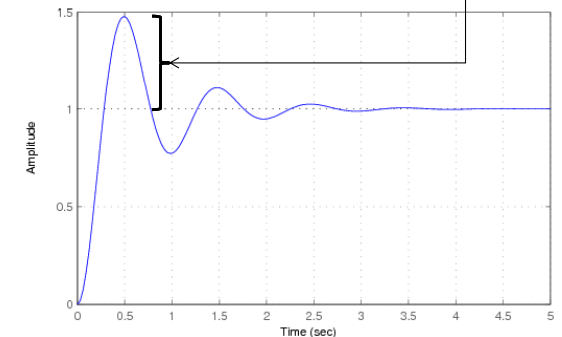
$$t_p = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}}$$

Rise Time and Overshoot

- Time duration between 10%-90% of the first peak of the damped oscillation
- Rule of thumb assuming $\zeta=0.5 \rightarrow t_r \approx \frac{1.8}{\omega_n}$

$$\text{at } t = t_p \quad 1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t_p} \sin(\omega_d t_p + \phi) = 1 + PO$$

Generic 2nd order response with DCG=1



Overshoot

$$1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t_p} \sin(\omega_d t_p + \phi) = 1 + PO$$

$$\omega_n t_p = \frac{\pi}{\sqrt{1-\zeta^2}}$$

$$\omega_d t_p = \pi$$

$$-\frac{1}{\sqrt{1-\zeta^2}} e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} \sin(\pi + \phi) = PO$$

$$\sin \pi + \phi = -\sin \phi = \sqrt{1-\zeta^2}$$

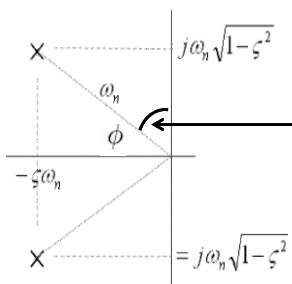
$$\frac{1}{\sqrt{1-\zeta^2}} e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} \sqrt{1-\zeta^2} = PO$$

$$e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} = PO$$

$$-\frac{\zeta\pi}{\sqrt{1-\zeta^2}} = \ln PO$$

$$\tan \beta = -\frac{\ln PO}{\pi}$$

$$\beta = \tan^{-1} \left\{ -\frac{\ln PO}{\pi} \right\}$$



$$\beta = \pi/2 - \phi$$

Settling Time

- Time for amplitude to drop to 1% of the original amplitude

$$y(t) = 1 - \frac{e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} \sin(\omega_d t + \phi)$$

$$e^{-\zeta\omega_n t_s} \approx 0.01$$

$$-\zeta\omega_n t_s \approx \ln 0.01$$

$$t_s \approx \frac{4.6}{\zeta\omega_n}$$

Design Conditions

maximum overshoot PO_{max} is specified

$$\beta > \tan^{-1} \left\{ -\frac{\ln PO_{max}}{\pi} \right\}$$

maximum settling time $t_{s,max}$ is specified

$$\zeta\omega_n > \frac{4.6}{t_{s,max}}$$

response has to rise before a maximum time of $t_{r,max}$

$$\omega_n > \frac{1.8}{t_{r,max}}$$